

HYDRAULIC FRACTURING EFFECTIVENESS ASSESMENT IN TIGHT RESERVOIRS AND MAIN CONSIDERATIONS FOR TREATMENT DESIGN AND PLANNING

- **María Florencia Melendo**
- **Miguel Jardel**
- **Santiago Casala**
- **Gustavo Kruse**

AGENDA

- 1- SUMMARY.
- 2- INTRODUCTION.
- 3- LOCATION, FORMATION.
- 4- DIAGNOSTIC PUMPINGS.
- 5- PETROPHYSICS AND GEOMECHANICS.
- 6- HYDRAULIC FRACTURING.
- 7- DESIGN.
- 8- FRACTURE HEIGHT ASSESSMENT AND HF SIMULATOR MATCHING.
- 9- FRACTURE SIMULATION RESULTS.
- 10- CONCLUSIONS.



1-Summary

- Incentives for hydrocarbon production.
- Analysis of the effectiveness of stimulation treatments.
- New hydraulic fracture design.
- Relevant information – Well logs and post-operation analysis.
- Case study in Magallanes formation of the Austral Basin.
- Conclusions about the propagation of hydraulic fractures.



2-Introduction

- Evolution of hydraulic fracturing treatments.
- Vertical and horizontal wells.
- Vertical wells – Design based in statistics or the best design to produce.
- Horizontal wells – Lateral section has increased in length.
- Horizontal wells – Increasing number of stages.
- Analysis of the effectiveness of stimulation treatments.
- Factors that affect final geometry.
- New hydraulic fracture design.

3-Location-Formation



CHARACTERISTICS	MAGALLANES M1 Formation
Location	Campo Indio Field. 140 km northwest of Río Gallegos city.
Reservoir	Magallanes is gas producer with associated condensate.
Rock	Sandstone
Depth (m)	1380-1500
Temperature (°F)	150-165
Permeability (mD)	0.1-1 (Tight facies)
Fracture Gradient (psi/ft)	0.55-0.63
Closure Gradient (psi/ft)	0.50-0.55



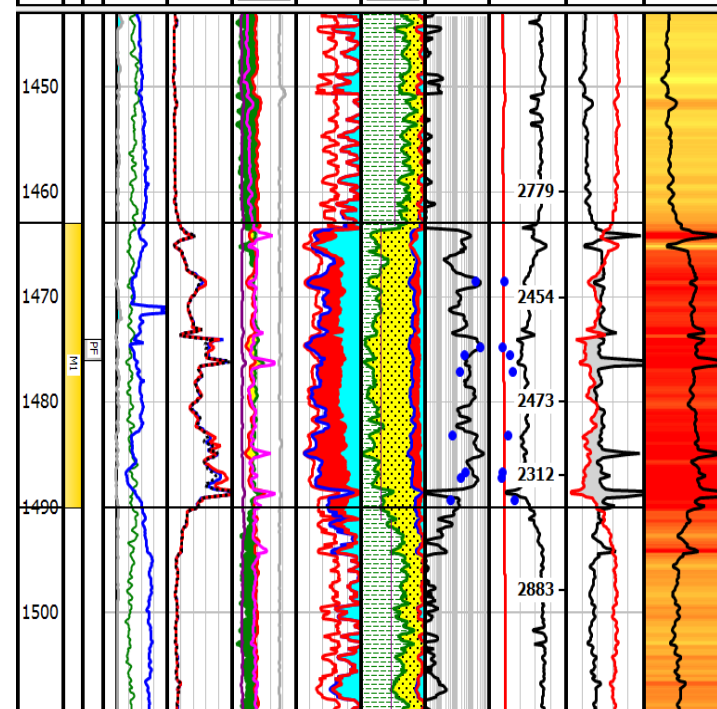
4-Diagnostic Pumpings

- DFIT-Water and Linear gel at low rates (Range 6-10 bbl/min).
- MINIFRAC-Linear gel at rates of the final treatment (Range 14-24 bbl/min).
- DFIT Objectives – Closure pressure, fluid efficiency, permeability (simulator matching).
- Minifrac Objectives – Perforations frictions and tortuosity (Step Down Rate Test). An estimation of fluid efficiency.

5-Petrophysics and Geomechanics

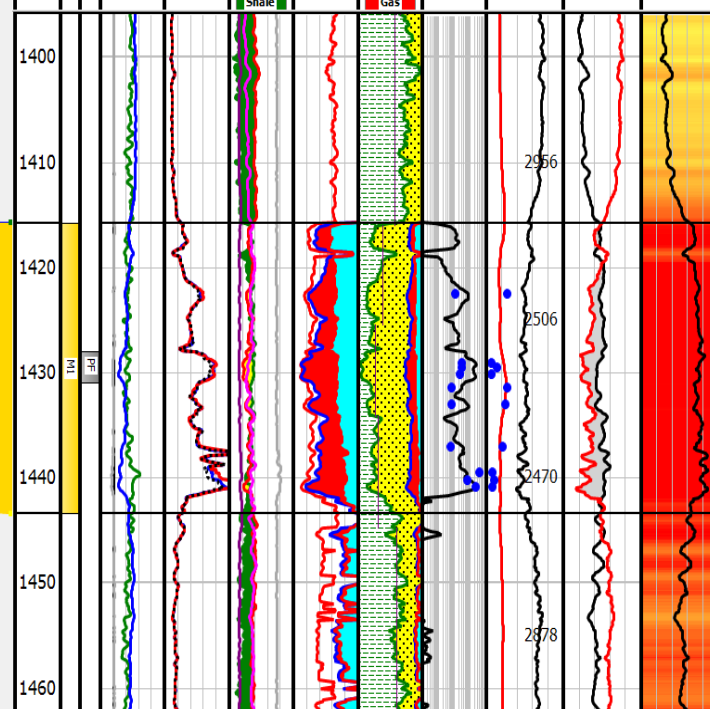
CI-69

CI-69											
MD	ZN	PF	Correlation	Resistivity	Porosity	Volumetric	Lithology	Permeability	Stresses/Press	YH-PR	PseudoBrit
DEPTH (M)	1st	Performations	GR (gAPI) 0. — 150. BS (in) 4. — 14. CAL 4. — 14. SP (mV) -445. -465. Washout Mudcake	AT60 0. — 10. AT90 0. — 10. AT30 0. 10.	TNPH LIM 0.45 - 0.15 RHOZ 1.95 + 2.95 DTC (us/ft) 140. — 40. PEFZ (B/E) 0. — 20. HDRA -0.75 0.25 Sand Shale	PHIT 0.3 — 0. PHIE 0.3 — 0. PhiSwr:BVW 0.3 — 0. Hyd Water Sandstone Clay Water Gas	VWVL 0. — 1. PHIE 1. — 0. PhiSwr:BVW 1. — 0. Clay Sandstone Clay Water Gas	Perm:Perm 0.001 + 10. DD Mobil 0.001 10	PPore:PP_Son 1500. — 3500. SHMINP 1500. — 3500. FM Pressure 1500 — 3500 Shmin	ESTR 0.25 — 2.25 PRSTA 0.15 — 0.45 PR-YH	BRIT 0 — 100 BRIT 0 — 100



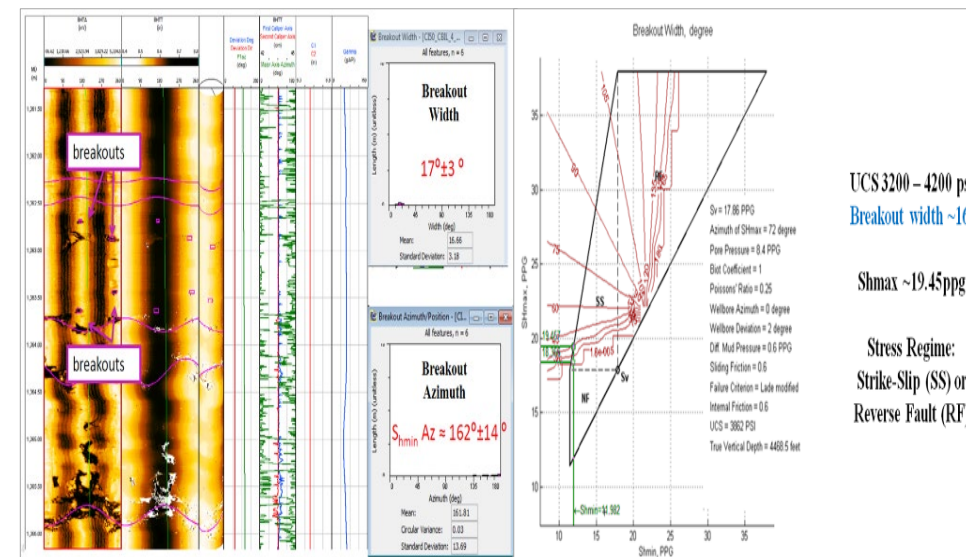
CI-88

CI-88												
MD	ZN	PF	Correlation	Resistivity	Porosity	Volumetric	Lithology	Permeabil	StressPress	YH-PR	PseudoBrit	
DEPTH (H)	M	Perforations	GR (gAPI)	0.	AT60	TNPH LI	PHIT	VWCL	Perm	PP Son	ESTA	BRIT:BRIT
			0. - 150.	0. - 10.	0.45 - 0.15	0.3	0. - 1.	0.001 10.	1500. 3500.	0.25 - 2.	0 100	
			BS (m)	AT90	RHOZ	PHIE	0.	DD Mobil	SHMINP	PRSTA	BRIT:BRIT	
			4. - 14.	0. - 10.	1.95 2.95	0.3	0. - 1.	1500. 3500.	0.17 - 0.45	0 - 100		
			CALI (in)	AT30	DTCO	BWW	BWW	SHMINP				
			4. - 14.	0. 10.	140. - 40.	0.3	0. - 1.	(psi)				
			SP (mV)		PEFZ	Hyd	Clay	FM Pressure				
			-240 -300.		0. - 20.	Water	Sand	1500 3500				
			Washout		HDRA							
			-240 -300.		-0.75 0.25							
		Mudcake	Sand	Water								



Formation Properties

Parameters	CI-69(d)	CI-88
Closure pressure (psi)	2420	2575
Closure pressure gradient (psi/ft)	0.512	0.55
Pore pressure (psi)	1930	1650
Pore pressure gradient (psi/ft)	0.41	0.35
Porosity (%)	5 - 15	5 - 15
Temperature (°F)	160	157





6-Hydraulic Fracturing

- Sandstone of low permeability (average range: 0.1 - 1 mD)
- Low contrast downwards of the stimulation average depth.
- Assessment in two wells.

Proppant and Fluid Volume: Well CI-69(d)					
Proppant	Sacks	%	System	gal	m ³
Mesh 100	75	2	Linear gel	8,176.00	31
Proppant 20/40	2112	64	Gel XL	82,700.00	313
Ceramic 20/40	1110	34			
Total	3297	100	Total	90,876.00	344

Proppant and Fluids Volume - Well CI-88					
Proppant	Sacks	%	System	gal	m ³
Ceramic 20/40	2,125	69	Linear gel	7,701	29
NRT 20/40	955	31	Gel XL	74,700	283
Total	3,080	100	Total	82,401	312



6-Hydraulic Fracturing

Hydraulic Simulation Treatment - Well CI-69(d)

Stage	Fluid System	Rate	Volume	Concentration		Proppant			Cumulative	
		bpm	gal	ppg	ppg	Type	Sacks	Sacks	gal	
Treatment										
PrePad	Linear gel	4	2000							5000
PrePad	Linear gel	8	2000							7000
Pad	XL gel	12	2000					0	0	9000
Pad	XL gel	18	15000	0.5	0.5	Mesh 100		75	75	24000
Pad	XL gel	18	4000					0	75	28000
Proppant	XL gel	18	3000	1	1	Sand 20/40		30	105	31000
Proppant	XL gel	18	3000	2	2	Sand 20/40		60	165	34000
Proppant	XL gel	18	4000	3	3	Sand 20/40		120	285	38000
Proppant	XL gel	18	10000	4	4	Sand 20/40		400	685	48000
Proppant	XL gel	18	10000	5	5	Sand 20/40		500	1185	58000
Proppant	XL gel	18	10700	6	6	Sand 20/40		642	1827	68700
Proppant	XL gel	18	6000	6	6	Sand 20/40	C.E.*	360	2187	74700
Proppant	XL gel	18	9000	6	8	NRT 20/40	C.E.*	630	2817	83700
Proppant	XL gel	18	6000	8	8	NRT 20/40	C.E.*	480	3297	89700
Displacement	Linear gel	18	1176							90876

*C.E. - Conductivity enhancer



6-Hydraulic Fracturing

Hydraulic Stimulation Treatment - Well CI-88

Stage	Fluid System	Rate	Volume	Concentration		Proppant			Cumulative	
		bpm	gal	ppg	ppg	Type		Sacks	Sacks	gal
Previous Tests										5240
Treatment										
PrePad	Linear gel	4	1500							6740
PrePad	Linear gel	8	1500							8240
Pad	XL gel	12	2000							10240
Pad	XL gel	18	13000							23240
Proppant	XL gel	18	1500	1	1	Ceramic 20/40		15	15	24740
Proppant	XL gel	18	3000	2	2	Ceramic 20/40		60	75	27740
Proppant	XL gel	18	4000	3	3	Ceramic 20/40		120	195	31740
Proppant	XL gel	18	6000	4	4	Ceramic 20/40		240	435	37740
Proppant	XL gel	18	11000	4	6	Ceramic 20/40		550	985	48740
Proppant	XL gel	18	19000	6	6	Ceramic 20/40		1140	2125	67740
Proppant	XL gel	18	9700	6	6	Ceramic 20/40	C.E.*	582	2707	77440
Proppant	XL gel	18	4000	6	7	NRT 20/40	C.E.*	260	2967	81440
Proppant	XL gel	18	1500	7	8	NRT 20/40	C.E.*	113	3080	82940
Displacement	Linear gel	18	1141							84081

*C.E. – Conductivity enhancer

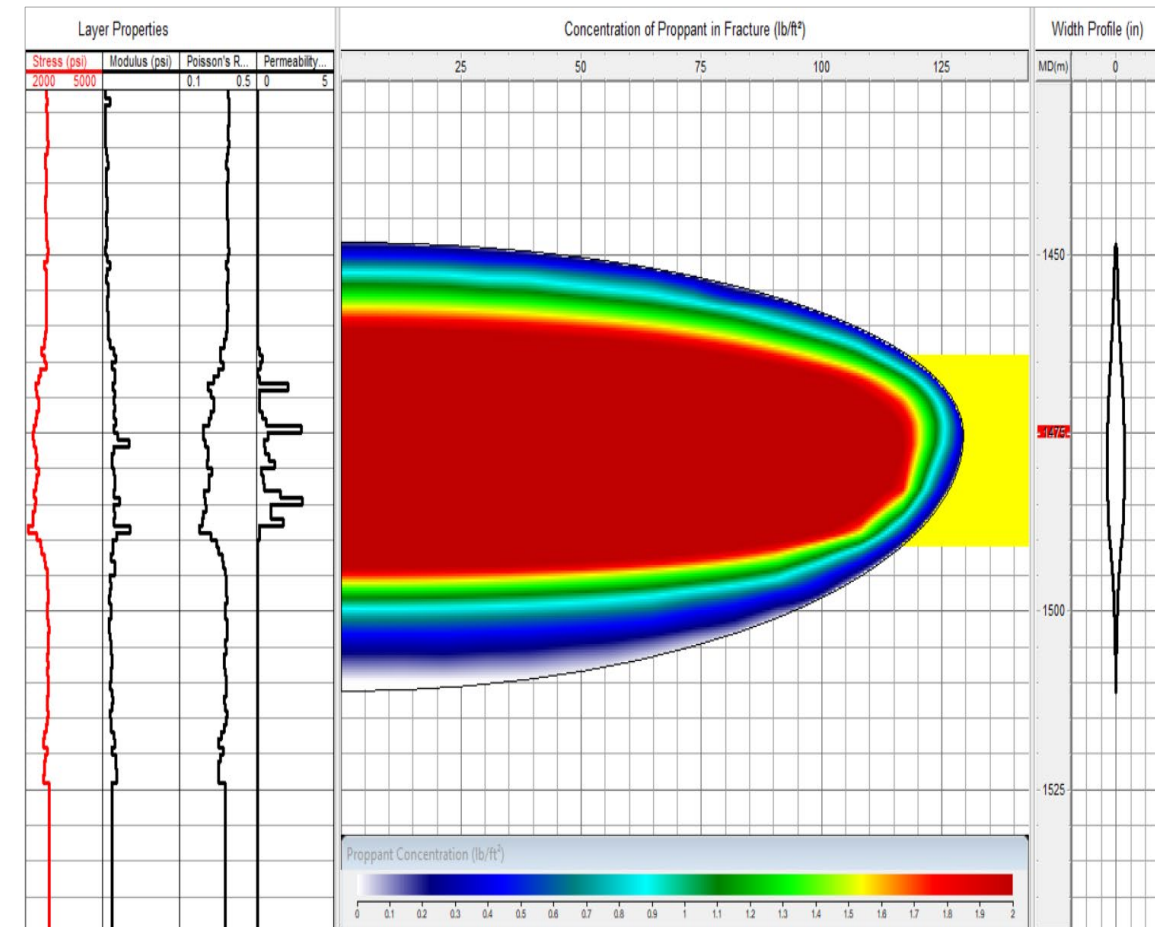
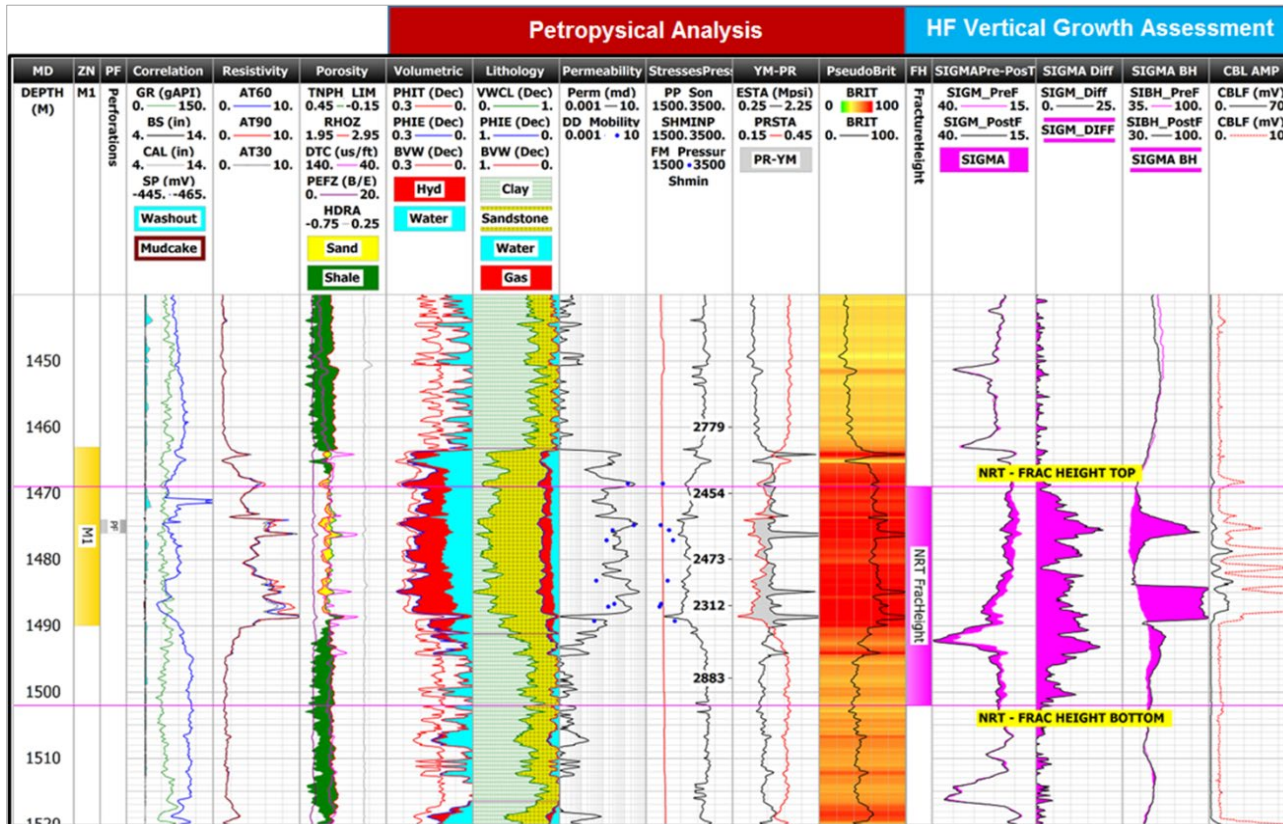


7-Design

Reservoir and Fracture Parameters - Design					
Reservoir	Well CI-69(d)	Well CI-88	Fracture	Well CI-69(d)	Well CI-88
Reservoir pressure	1930 psi	1,650 psi	Fracture length	134.50 m	122.60 m
Reservoir pressure gradient	0.41 psi/ft	0.35 psi/ft	Proppant length	102.90 m	108.50 m
Total compressibility	1.39E-4 1/psi	2.60E-4 1/psi	Total fracture height	65.32 m	57.21 m
Permeability	0.01 – 0.10 mD	0.01 – 0.10 mD	Total proppant height	49.89 m	50.63 m
Closure stress pressure	2420 psi	2575 psi	Average fracture width	0.292 in	0.305 in
Closure stress gradient	0.512 psi/ft	0.55 psi/ft	Proppant concentration	2.346 lb/ft ²	2.623 lb/ft ²



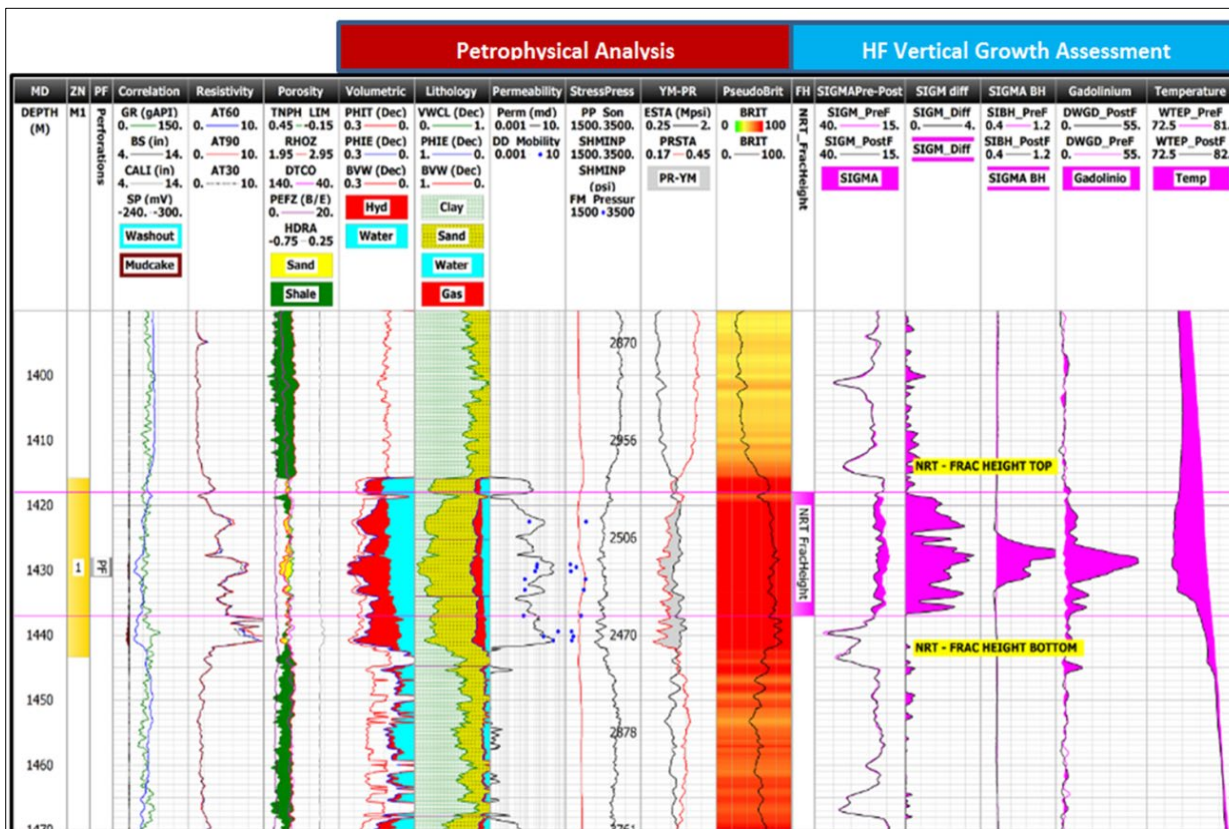
8-Fracture Height Assessment and HF Simulator Matching – Well CI-69(d)



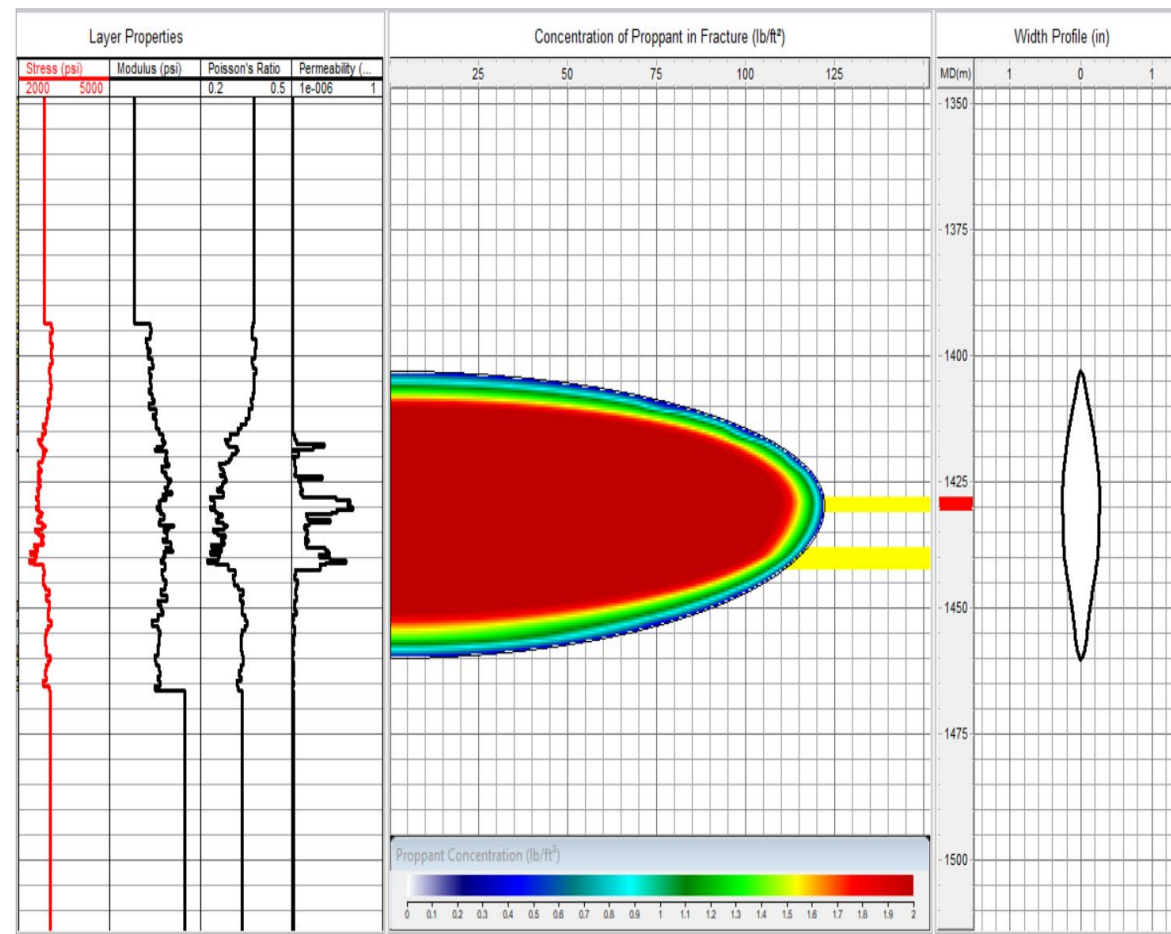
HF Stimulation Treatment Matching - Well CI-69(d)

M1 Gross Interval (mMD)	Perforated Interval (mMD)	Interval w/NRT (mMD)	HF Simulator Matching (mMD)
1463.5	1492.5	1474.0	1476.0
1470.0	1502.0	1469.0	1504.0

8-Fracture Height Assessment and HF Simulator Matching – Well CI-88

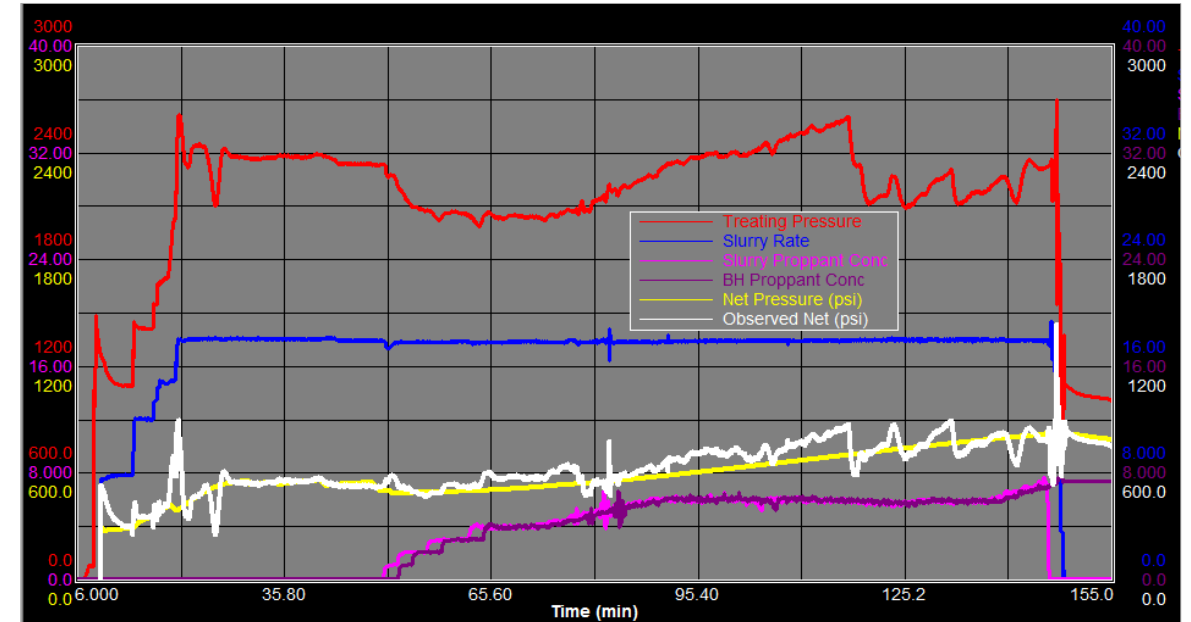
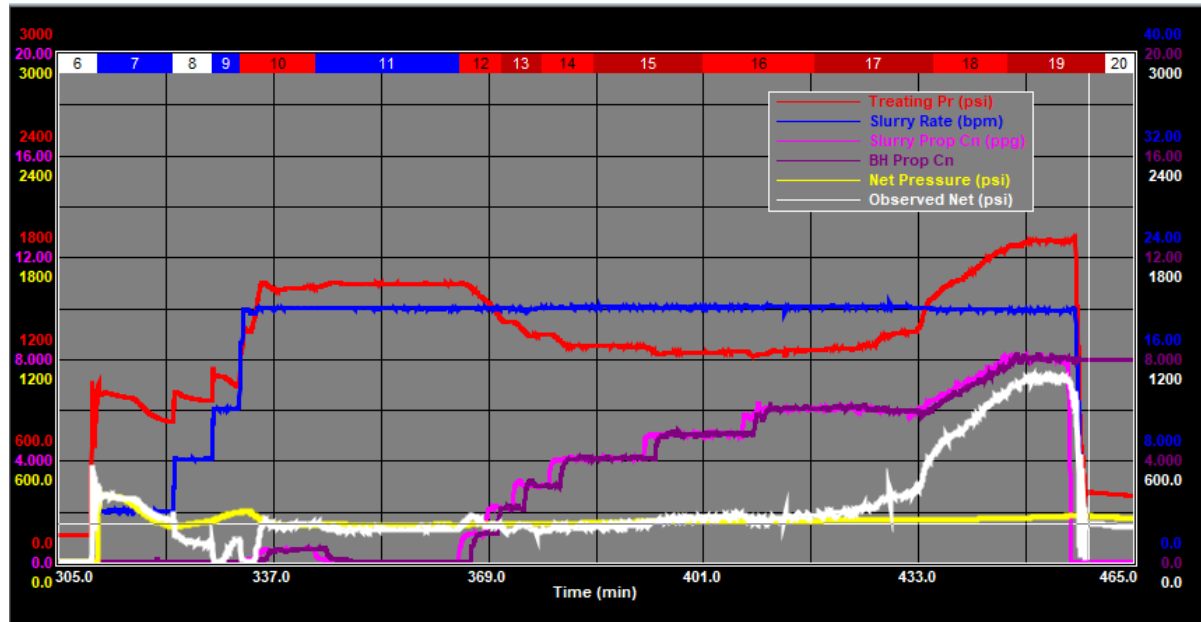


HF Stimulation Treatment Matching Well CI-88							
M1 Gross Interval (mMD)		Perforated Interval (mMD)		Interval w/NRT (mMD)		HF Simulator Matching (mMD)	
1416.0	1445.0	1428.0	1431.0	1418.7	1436.7	1406.0	1456.0





9-Fracture Simulation Results



Pre- and Post-HF Treatment Parameters Comparison - Wells CI-69(d) and CI-88								
Well	Rate (bpm)	Proppant (sacks)	ISIP Prefrac (psi)	Initial Fracture Gradient (psi/ft)	ISIP Post-frac (psi)	Final Fracture Gradient (psi/ft)	ISIP Variation (psi)	ISIP Variation (%)
CI-69(d)	20	3,303	660	0.58	415	0.52	-245	-37%
CI-88	18	3,044	590	0.56	1,095	0.67	505	86%



10-Conclusions

- The difference in the ISIPs explains the observed results in terms of the extension of the vertical growth.
- The use of a low density ceramic proppant contributed to the expected production.
- The cement quality condition is believed to be the cause of the difference observed between the vertical growths of both HF stimulations.
- The results indicate that the rock properties, low density ceramic proppant, and the cement conditions affect the final geometry registered in the appropriate profiles.

Questions?